

Chapter 2. Specifications

INTRODUCTION

This chapter provides information on the stand-alone specifications and characteristics of the analyzer, and on the specified and typical performance of the analyzer system. The analyzer system consists of the analyzer plus the test cable supplied with (and matched to) the analyzer.

ANALYZER SPECIFICATIONS AND CHARACTERISTICS

Table 2-1 lists specifications and typical characteristics of the stand-alone analyzer (without its matched cable). Specifications are the performance standards or limits against which the instrument can be tested. They are field verifiable using performance tests documented in the service manual.

Typical characteristics are not specifications but are non-warranted performance characteristics provided for use in applying the instrument. Typical characteristics are representative of most instruments, though not necessarily factory-tested in each unit. They are not field tested.

Table 2-2 lists supplemental characteristics of the instrument. These are general descriptive information provided for use in applying the instrument.

SYSTEM SPECIFICATIONS AND SYSTEM PERFORMANCE

Table 2-3 lists measurement port specifications for the system (analyzer and matched cable). These specifications are the residual system uncertainties with and without error correction.

The last part of this chapter explains system performance and residual measurement errors. It provides a description of error sources, graphs of typical measurement uncertainty, and information on determining expected performance for a particular system.

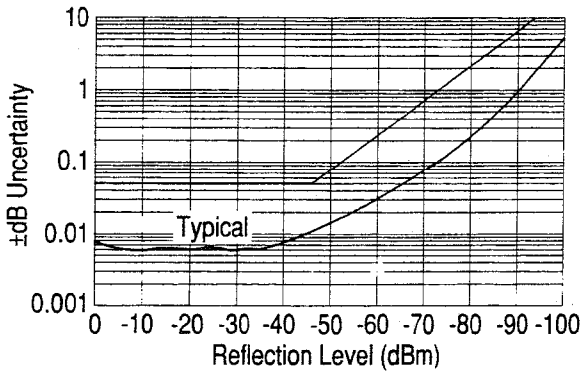
Table 2-1. Instrument Specifications (1 of 2)

Specifications describe the instrument's warranted performance over the temperature range of 0 ° to 55 °C (except where noted). Figures denoted as typical are not specifications but are non-warranted performance parameters provided for use in applying the instrument.			
SOURCE¹			
Frequency		Output Power	
Range:	standard 300 kHz to 1.3 GHz option 003 300 kHz to 3 GHz	Test port power range:	–20 to +5 dBm
Resolution:	1 Hz	Resolution:	0.1 dB
Stability:	typically ± 7.5 ppm 0 to 55 °C typically ± 3 ppm/year	Flatness ² :	2 dB Peak to Peak
Accuracy:	10 ppm at 25 °C ± 5 °C	Level accuracy ² :	± 0.5 dB at 50 MHz
		Level linearity ² :	± 0.5 dB from –20 to –15 dBm ± 0.2 dB from –15 to 0 dBm ± 0.5 dB from 0 to +5 dBm
RECEIVER¹			
Input			
Frequency range:	Standard 300 kHz to 1.3 GHz Option 003 300 kHz to 3 GHz	Maximum input level:	0 dBm at Transmission Port 10 dBm at Reflection Port
Dynamic range ³ :	100 dB	Damage Level:	20 dBm or >25 VDC at Transmission Port 30 dBm or >25 VDC at Reflection Port
Noise level:	3 kHz BW Reflection –75 dBm (typical) 10 Hz BW Reflection –85 dBm (typical) 3 kHz BW Transmission –90 dBm 10 Hz BW Transmission –100 dBm (typically –110 dBm)	Crosstalk: (Reflection Port to Transmission Port)	300 kHz to 1.3 GHz: 100 dB 1.3 to 3 GHz: 90 dB
Magnitude		Phase	
Dynamic accuracy:	Refer to Figure 2-1a.	Dynamic accuracy:	Refer to Figure 2-1b.
Display resolution:	0.01 dB/div.	Range:	± 180 degrees
Marker resolution ³ :	0.001 dB	Frequency response (deviation from linear, –10 dBm, 25 ° ± 5 °C):	± 3 °
Trace noise:	(0 dBm, 3 kHz BW; reflection): <0.006 dB rms (0 dBm, 3 kHz BW; transmission): <0.006 dB rms	Display resolution:	0.01 °/div.
Reference level:	range: ± 500 dB resolution: 0.001 dB	Marker resolution ³ :	0.01 °
Stability:	0.02 dB/°C typically	Trace noise:	(0 dBm, 3 kHz BW; reflection): <0.035 ° rms (0 dBm, 3 kHz BW; transmission): <0.035 ° rms
		Reference level: range:	± 500 degrees
		Stability:	resolution: 0.01 degrees 0.1 °/°C typically
<p>1. HP 8752B option 003 specifications above 2 GHz are typical due to 75 ohm measurement standards having an upper frequency limit of 2 GHz</p> <p>2. At 25 °C ± 5 °C relative to –5 dBm test port power.</p> <p>3. This specification applies to transmission measurements in the 300 kHz to 1.3 GHz frequency range at 10 Hz IF bandwidth with response and isolation correction. Dynamic range is limited by maximum receiver input level and system noise floor.</p> <p>4. Marker resolution is dependent upon the value measured; resolution is limited to five digits.</p>			

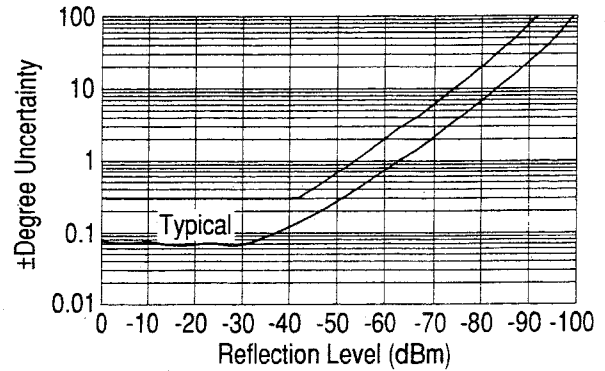
Table 2-1. Instrument Specifications (2 of 2)

DYNAMIC ACCURACY

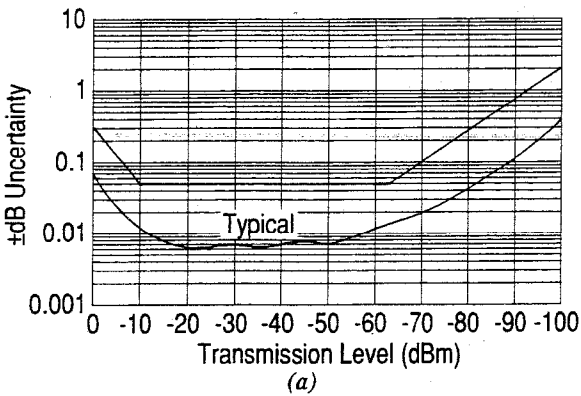
Dynamic accuracy: Transmission



Dynamic accuracy: Reflection (Typical):



Dynamic accuracy: Transmission



Dynamic accuracy: Reflection (Typical):

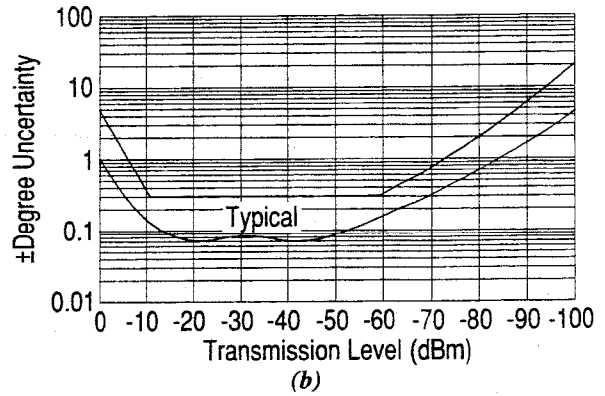


Figure 2-1. Receiver Dynamic Accuracy

Dynamic accuracy for both reflection (typical) and transmission (specified) is determined from the plots in Figure 2-1. The power along the x-axis is expressed in dBm and is equivalent to the power at the transmission port for transmission measurements. For reflection measurements it is the power re-entering the reflection port after reflecting off the DUT.

Once the x-axis value is determined, read the corresponding dynamic accuracy from the plot.

Example: Reflection Dynamic Accuracy

(Refer to Figure 2-1b.)

Test port power: -10 dBm
DUT return loss: 20 dB
Reflected power = (test port power)
- (DUT return loss)
= (-10 dBm) - (20 dB)
= -30 dBm
Reflection Dynamic Accuracy at -30 dBm: ± 0.06 dB

Example: Transmission Dynamic Accuracy

(Refer to Figure 2-1a.)

Test port power: -10 dBm
DUT insertion loss: 10 dB
Transmitted power = (test port power)
- (DUT insertion loss)
= (-10 dBm) - (10 dB)
= -20 dBm
Transmission Dynamic Accuracy at -20 dBm: ± 0.05 dB

Table 2-2. Supplemental Characteristics (1 of 4)

These are not specifications, but general descriptive information provided for use in applying the instrument.

MEASUREMENT THROUGHPUT SUMMARY

The following shows typical measurement times in milliseconds.

Typical time for completion (msec)

	Number of Points			
	51	201	401	1601
Measurement				
Uncorrected or 1-port cal ¹	120	190	290	890
2-port cal	540	1030	1680	5610
Time domain conversion²	125	540	1150	2840
HP-IB data transfer³				
Internal	30	50	75	660
ASCII	500	1900	3800	15000
IEEE 754 floating point format:				
32 bit, 32 bit MS-DOS [®]	40	85	140	500
64 bit	60	125	210	700

REMOTE PROGRAMMING

Interface

HP-IB interface operates according to IEEE 488-1978 and IEC 625 standards and IEEE 728-1982 recommended practices.

Transfer Formats

Binary (internal 48-bit floating point complex format)

CITIFile ASCII

32/64 bit IEEE 754 Floating Point Format

Interface Function Codes

SH1, AH1, T6, TE0, L4, LE0, SR1, RL1, PP0, DC1, DT1, C1, C2, C3, C10, E2

¹ Reflection 1-Port calibration with a 3 kHz IF BW. Includes system retrace time but does not include bandswitch time. Time domain gating is assumed off.

² Option 010 only, gating off.

³ Measured with HP 9000 Series 300 computer

MS-DOS[®] is a U.S. registered trademark of Microsoft Corporation.

Table 2-2. Supplemental Characteristics (2 of 4)

GROUP DELAY CHARACTERISTICS

Group delay is computed by measuring the phase change within a specified frequency step (determined by the frequency span, and the number of points per sweep).

Aperture: Selectable

Maximum aperture: 20% of frequency span

Minimum aperture: (frequency span)/(number of points - 1)

Range:

The maximum delay is limited to measuring no more than 180° of phase change within the minimum aperture.

Range = $1/(2 \times \text{minimum aperture})$

Accuracy:

The following graph shows group delay accuracy at 1.3 GHz with an uncorrected measurement. IF BW is 10 Hz. Insertion loss is assumed to be small and device electrical length is 10 meters.

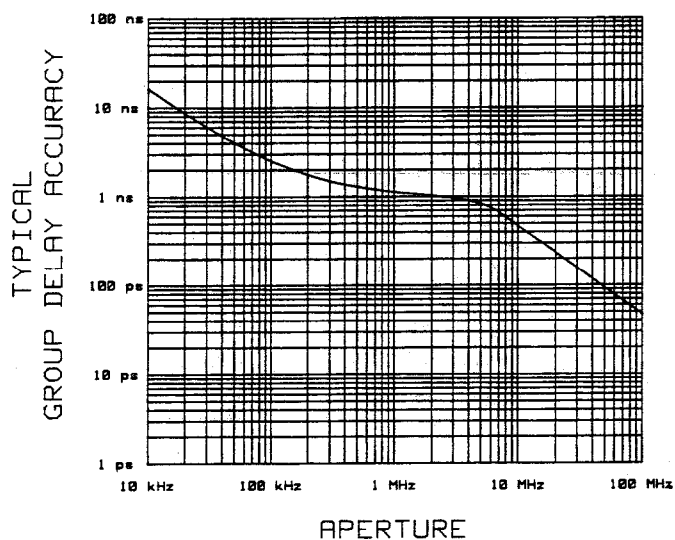


Figure 2-2. Group Delay Accuracy at 1.3 GHz

In general, the following formula can be used to determine the accuracy, in seconds, of a specific group delay measurement.

$$\pm (0.003 \times \text{Phase accuracy(deg)}) / \text{Aperture(Hz)}$$

Depending on the aperture and device length, the phase accuracy used is either incremental phase accuracy or worst case phase accuracy. The above graph shows this transition.

Table 2-2. Supplemental Characteristics (3 of 4)

FRONT PANEL CONNECTORS

	HP 8752A	HP 8752B
Connector Type	type-N (female)	type-N (female)
Impedance	50 ohms (nominal)	75 ohms (nominal)
Connector Pin Protrusion	0.204 to 0.207 in	0.204 to 0.207 in

REAR PANEL CONNECTORS

External Reference Frequency Input (EXT REF INPUT)

Frequency	1, 2, 5, and 10 MHz (± 200 Hz @ 10 MHz)
Level	-10 dBm to +20 dBm, typical
Impedance	50 ohms

External Auxiliary Input (AUX INPUT)

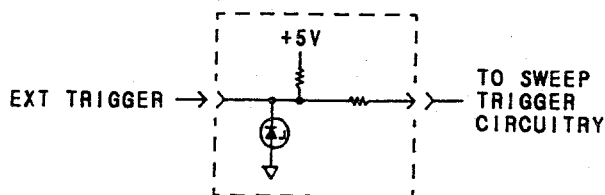
Input Voltage Limits -10V to +10V

External AM Input (EXT AM)

± 1 volt into a 5k ohm resistor, 1 kHz maximum, resulting in 8 dB/volt amplitude modulation.

External Trigger (EXT TRIGGER)

Triggers on a negative TTL transition or contact closure to ground.



External Trigger Circuit

LINE POWER

47 to 66 Hz
115V nominal +10% -25% or 230V +10% -15%. 220 VA max.

PROBE POWER

+15V $\pm 2\%$, 400 mA
-12.6V $\pm 5.5\%$, 300 mA

ENVIRONMENTAL REQUIREMENTS

Operating Conditions

Temperature	0 to 55°C
Humidity	Operate in a non-condensing environment
Altitude	0 to 4500 meters (15,000 feet)

Table 2-2. Supplemental Characteristics (4 of 4)

Non-Operating Storage Conditions

Temperature	-40°C to +70°C
Humidity	Store in a non-condensing environment
Altitude	0 to 15,240 metres (50,000 feet)

WEIGHT

Net	25.4 kg (56 lb)
Shipping	28.4 kg (63 lb)

CABINET DIMENSIONS

178 H x 425 W x 497.8 mm D
(7.0 x 16.75 x 19.0 in)

(These dimensions exclude front and rear panel protrusions. Add 24 mm (1 in) to depth to include the front panel connectors.)

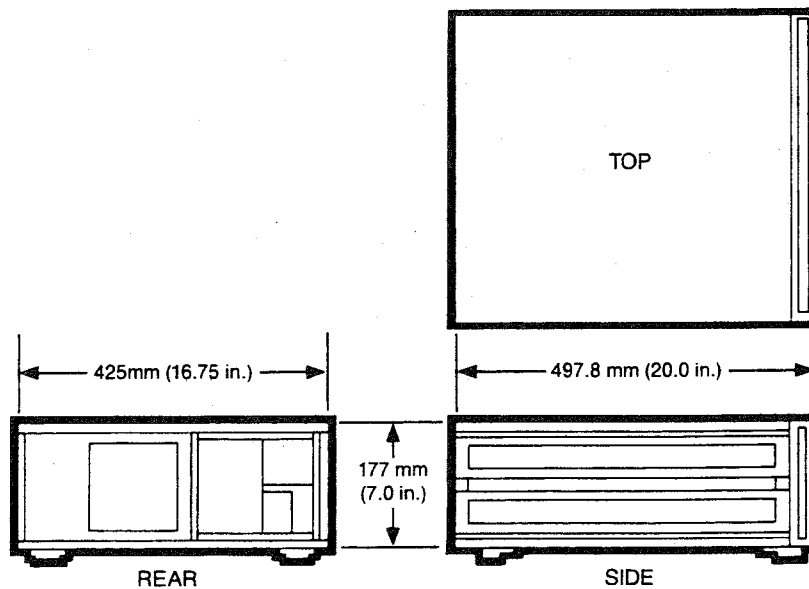


Table 2-3. System Specifications

MEASUREMENT PORTUNCERTAINTIES

The following specifications show the residual system uncertainties with and without error correction. The system is defined as the analyzer plus its matched cable. When two values are given for one specification (for example: 40/35), the number on the left applies up to 1.3 GHz, the number on the right applies from 1.3 to 3 GHz.

NOTE: All HP 8752B option 003 specifications above 2 GHz are typical due to 75 ohm measurement standards having an upper frequency limit of 2 GHz.

Error Term	Uncorrected ¹		3.5 mm ^{2,3}		Type-N ³	
	dB	Linear	dB	Linear	dB	Linear
Directivity	-40/-35 ⁴	0.01/0.0178	-40	0.01	-44	0.0063
Reflection Tracking	±0.2/±0.3	0.0233/ 0.0351	±0.06	0.0069	±0.06	0.0069
Transmission Tracking	±0.2/±0.3	0.0233/ 0.351	±0.05/ ±0.1	0.0058/ 0.0116	±0.05/ ±0.1	0.0058/ 0.0116
Source Match (reflection)	-30/-25	0.0316/ 0.0562	-36	0.0158	-35	0.0178
Source Match (transmission)	-23/-20	0.0708/0.1	-23/-20	0.0708/0.1	-23/-20	0.0708/0.1
Load Match	-23/-20	0.0708/0.1	-23/-20	0.0708/0.1	-23/-20	0.0708/0.1
Crosstalk	-100/-90	0.00001/ 0.00003	-100/-90	0.00001/ 0.00003	-100/-90	0.00001/ 0.00003
Connector Repeatability (typical)	-65	0.0006	-70	0.0003	-65	0.0006
Error Term			dB		Linear	
Noise Floor ⁵ , Transmission: (Included in dynamic accuracy)			-100 (10 Hz BW)		0.00001	
Trace Noise			0.006 dB rms		0.0007	
Cable Reflection Magnitude Stability (typical)			-60 dB		0.001	
Error Term			Degrees			
Cable Transmission Phase Stability (typical):			0.05 x Frequency (in GHz) degrees			

1. These uncertainties apply in an environmental temperature of 23° ± 10/-5°C with an IF bandwidth of 10 Hz

2. HP 8752A only.

3. These uncertainties apply in an environmental temperature of 23° ± 3°C, with less than 1° deviation from the temperature at measurement calibration. IF BW is 10 HZ.

4. -30 dB from 300 kHz to 10 MHz.

5. Noise floor is already included in dynamic accuracy performance data.

SYSTEM PERFORMANCE

INTRODUCTION

System performance depends not only on the performance of the analyzer and the cables, but also on operating conditions and on measurement errors inherent in network analysis.

The following pages provide a brief description of the sources of measurement errors, graphs of typical measurement uncertainty for the HP 8752A and 8752B, and information to use in determining the expected performance of a particular system.

Also provided are tips on increasing dynamic range by reducing associated measurement errors.

INCREASING DYNAMIC RANGE

Dynamic range is limited by the maximum receiver input level (the high end of the range), and by either of these two factors on the minimum end of the range:

- System noise floor
- Crosstalk

Noise Floor

System noise floor can be reduced using a narrow IF bandwidth or with averaging, or with a combination of both. These measures can reduce noise floor below the crosstalk error level, making crosstalk error the limiting factor in dynamic range. A response and isolation calibration can then reduce the crosstalk errors. *The noise floor must be less than the crosstalk error or a response and isolation calibration will not reduce crosstalk errors.* The "Calibration" chapter explains how to determine which is greater: noise floor or crosstalk

Crosstalk

Crosstalk is a factor only in measurements requiring wide dynamic range. When crosstalk is greater than the noise floor, a response and isolation calibration can reduce its effects, thereby increasing dynamic range. However, if the noise floor is greater than crosstalk, the response and isolation cal will have no effect on dynamic range. The "Calibration" chapter explains this in detail.

SOURCES OF MEASUREMENT ERRORS

Network analysis measurement errors can be separated into the following types of errors:

- Systematic errors.
- Random errors.
- Drift errors.

Systematic Error Sources

The model for systematic errors is shown below. Refer to the end of the chapter for reflection uncertainty and transmission uncertainty equations derived from the system error model. Systematic errors result from imperfections in the calibration standards, connector standards, connector interface, interconnecting cables, and the instrumentation. All measurements are affected by dynamic accuracy.

Errors in Reflection Measurements. Directivity, source match, and reflection tracking are the errors that affect reflection measurements.

Errors in Transmission Measurements. Crosstalk, source match, load match, transmission tracking, and cable stability are the errors that affect transmission measurements.

Refer to the "Measurement Calibration" chapter for an explanation of each of these individual errors.

Random Error Sources

Non-repeatable errors are trace noise, noise floor (included in dynamic accuracy), and connector repeatability. These errors affect both transmission and reflection measurements.

Drift Errors

The effects of temperature drift are included in the system specifications data.

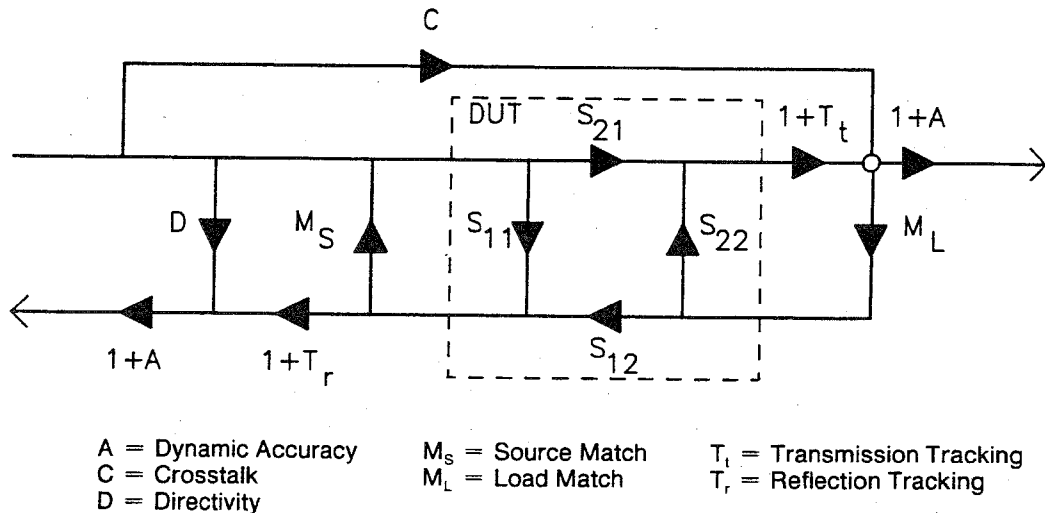


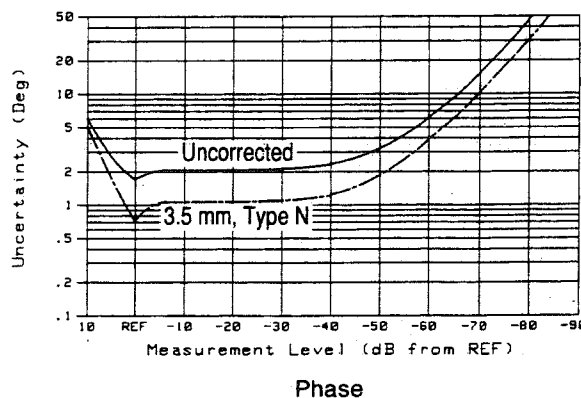
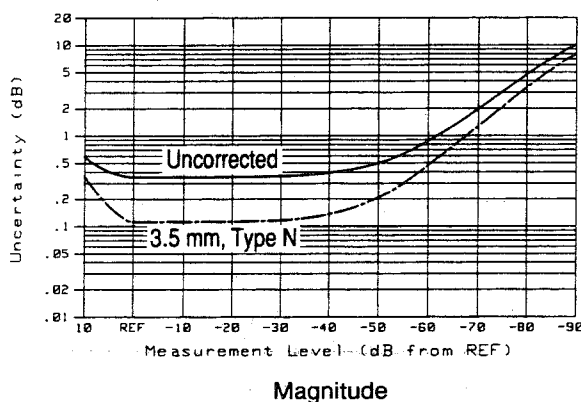
Figure 2-3. System Error Model

TYPICAL MEASUREMENT UNCERTAINTY FOR HP 8752A

The graphs¹ below show the typical measurement uncertainty for the analyzer using type-N or 3.5 mm connectors, with and without error correction. Two graphs are provided for transmission measurements (a magnitude graph and a phase graph), and two for reflection measurements. The graphs on the next page apply to the HP 8752A option 003.

Corrected performance in the transmission measurement graphs shows the improvement obtained from a response and isolation calibration. Corrected performance in the reflection measurement graphs shows the improvement obtained from a reflection 1-port calibration.

Transmission measurements²



Reflection measurements³

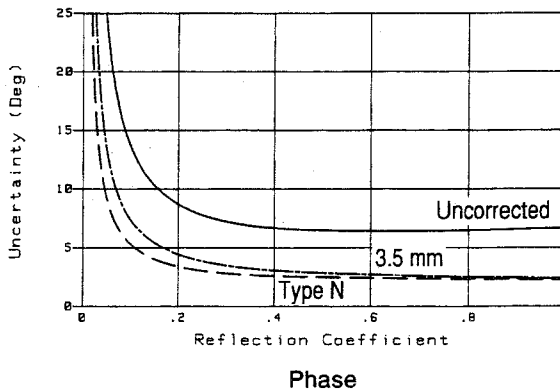
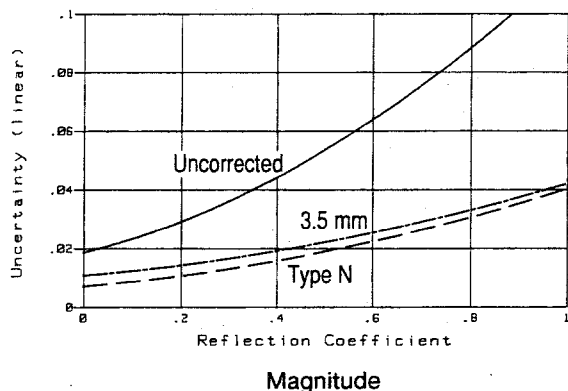
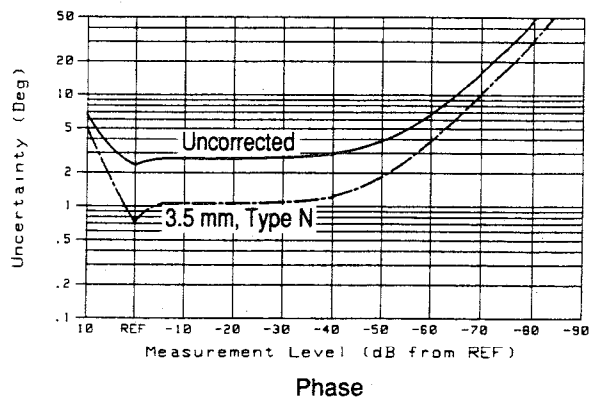
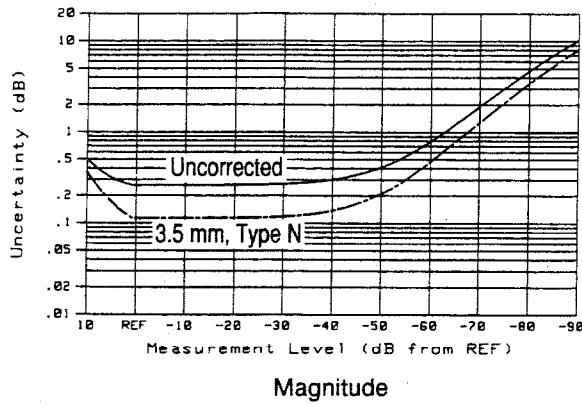


Figure 2-4. Typical Measurement Uncertainty for Standard HP 8752A (300 kHz to 1.3 GHz)

1. These measurement uncertainty curves utilize an RSS model for the contributions of random errors such as noise, and typical connector repeatabilities; and a worst-case model for the contributions of dynamic accuracy and residual systematic errors.
2. The graphs shown for transmission measurements assume a well-matched device ($S_{11} = S_{22} = 0$).
3. The graphs for reflection measurement uncertainty apply to either a one-port device or a two-port device with more than 6 dB of insertion loss.

Transmission measurements¹



Reflection measurements²

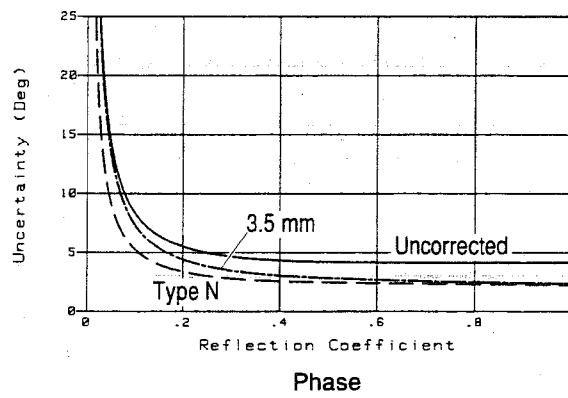
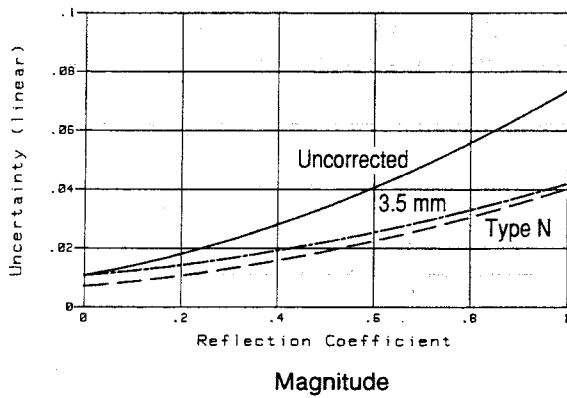


Figure 2-5. Typical Measurement Uncertainty for HP 8752A Option 003 (300 kHz to 3 GHz)

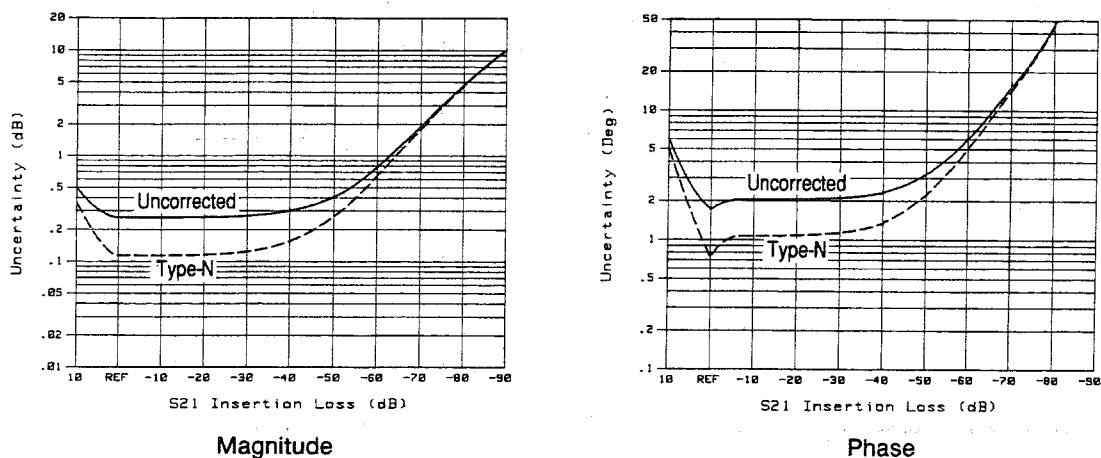
1. The graphs shown for transmission measurements assume a well-matched device ($S_{11} = S_{22} = 0$).
2. The graphs for reflection measurement uncertainty apply to either a one-port device or a two-port device with more than 6 dB of insertion loss.

TYPICAL MEASUREMENT UNCERTAINTY FOR HP 8752B

The graphs¹ below show the typical measurement uncertainty for the analyzer using type-N connectors, with and without error correction. Two graphs are provided for transmission measurements (a magnitude graph and a phase graph), and two for reflection measurements. The graphs on the next page apply to the HP 8752B option 003.

Corrected performance in the transmission measurement graphs shows the improvement obtained from a response and isolation calibration. Corrected performance in the reflection measurement graphs shows the improvement obtained from a reflection 1-port calibration.

Transmission measurements²



Reflection measurements³

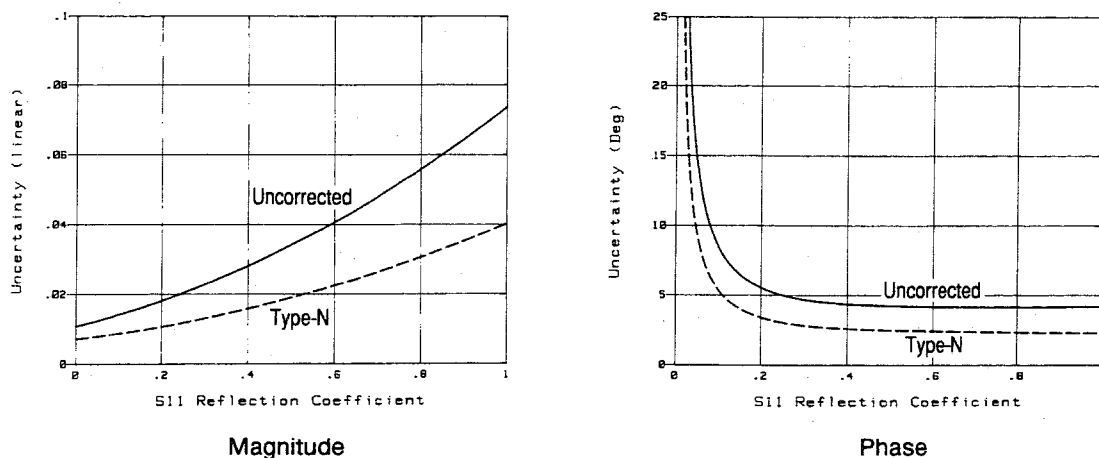
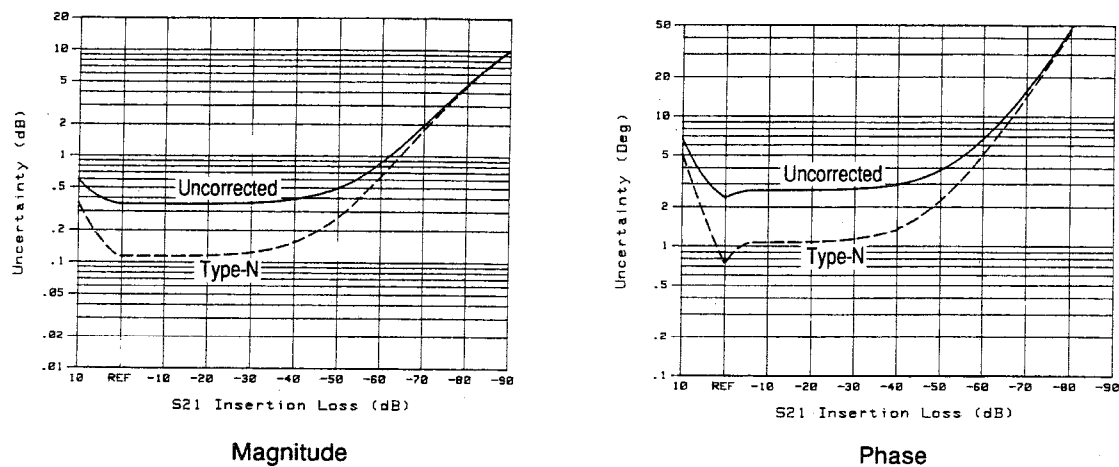


Figure 2-6. Typical Measurement Uncertainty for Standard HP 8752B (300 kHz to 1.3 GHz)

1. These measurement uncertainty curves utilize an RSS model for the contributions of random errors such as noise, and typical connector repeatabilities; and a worst-case model for the contributions of dynamic accuracy and residual systematic errors.
2. The graphs shown for transmission measurements assume a well-matched device ($S_{11} = S_{22} = 0$).
3. The graphs for reflection measurement uncertainty apply to either a one-port device or a two-port device with more than 6 dB of Insertion loss

Transmission measurements¹



Reflection measurements²

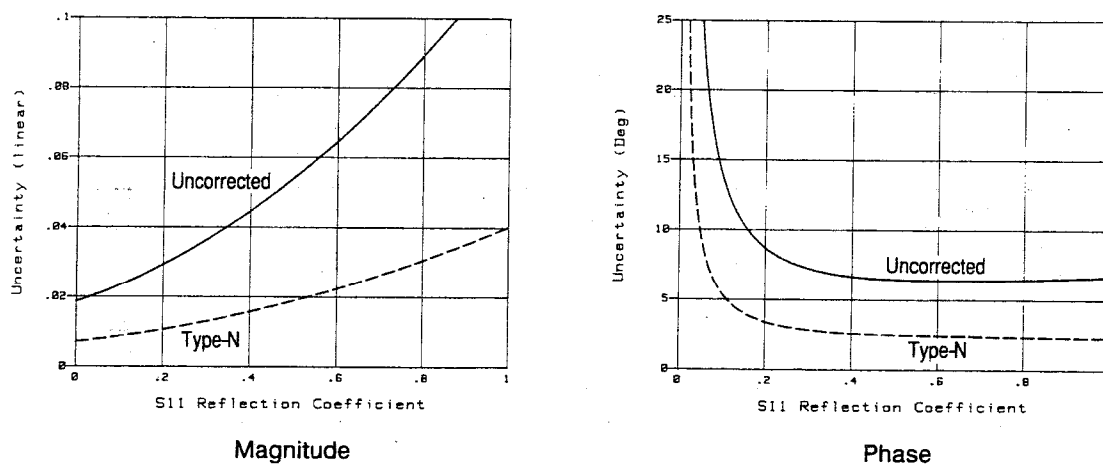


Figure 2-14. Typical Measurement Uncertainty for HP 8752B Option 003 (300 kHz to 3 GHz)

1. The graphs shown for transmission measurements assume a well-matched device ($S_{11} = S_{22} = 0$).
2. The graphs for reflection measurement uncertainty apply to either a one-port device or a two-port device with more than 6 dB of Insertion loss.

DETERMINING EXPECTED SYSTEM PERFORMANCE

The uncertainty equations and tables of system specifications provided in this chapter can be used to calculate the expected system performance of the analyzer. The following pages explain how to determine the residual errors of a particular system and combine them to obtain total error-corrected residual uncertainty values, using worksheets (Tables 2-4 and 2-5).

Separate tables are used to determine residual magnitude and phase uncertainties in the following measurement types:

- Table 2-4: Reflection measurements
- Table 2-5: Transmission measurements
- Completed examples of the residual uncertainty tables are provided after Table 2-5.

NOTE: A spreadsheet program can automate the uncertainty worksheets and eliminate mathematical errors.

Determining Crosstalk

The crosstalk error value is required in the transmission uncertainty worksheet. You can use the value in Table 2-3 or measure it as explained below:

Connect impedance-matched loads to the reflection and transmission ports. Set IF bandwidth to 10 Hz by pressing **[AVG] [IF BW] [10] [x1]**. Turn on an averaging factor of 5 by pressing **[AVERAGING FACTOR] [5] [x1] [AVERAGING ON]**. Averaging reduces the analyzer's noise floor as explained earlier in this section.

Select a transmission measurement, turn on the marker statistics function (see "Using Markers"), and measure the mean value of the trace. Use the mean value plus one standard deviation as the residual crosstalk value of your system.

Table 2-4. Reflection Measurement Uncertainty Worksheet

PART A – Analyzer Performance

Frequency: _____

In the columns below, enter the values for each term. Values are obtained from Table 2-3 and Figure 2-1.

Error Term	Symbol	dB Value	Linear Value
Directivity	D		_____
Reflection tracking	T _r		_____
Source match (reflection)	M _s		_____
Load match	M _l		_____
Dynamic accuracy			
Magnitude ¹	A _m	+ _____	_____
Phase	A _p		_____
Trace noise	N _n		_____
Connector repeatability	R _c		_____

PART B – DUT Performance

In the columns below, enter the calculated or measured performance of the DUT.

Performance Parameter	dB Value	Linear Value (10 ^{dB Value/20})
S11	_____	_____
S21	_____	_____
S12	_____	_____

PART C — Total Magnitude Errors (Systematic and Random)

Systematic Errors

In the spaces provided, enter the required linear values from Parts A and B. Then combine these errors to obtain the total sum of systematic errors.

D			=	_____ [k]
T _r x S11			=	_____ [l]
M _s x S11 x S11			=	_____ [m]
M _l x S21 x S12	x _____	x _____	=	_____ [n]
A _m x S11	x _____	x _____	=	_____ [o]
Total Systematic Errors: k + l + m + n + o			=	_____ [S]

Random Errors

Enter the required linear values from Parts A and B. Combine these errors in a root sum of the squares (RSS) fashion to obtain a total sum of random errors.

$$\begin{array}{lcl} 3 \times N_h \times S11 & 3x & x \\ R_c \times (1 + 2 \times S11 + S11^2) & x(1 + 2x + x^2) & = \\ R_c \times S21 \times S12 & x & x \end{array} \begin{array}{l} = \\ = \\ = \end{array} \begin{array}{l} [x] \\ [y] \\ [z] \end{array}$$

Total Random Errors

$$\sqrt{x^2 + y^2 + z^2} = \sqrt{\quad} + \sqrt{\quad} + \sqrt{\quad} = \quad [R]$$

TOTAL MAGNITUDE ERRORS:

$$E_{rm}(\text{linear}) = S + R \quad \underline{\hspace{1cm}} + \underline{\hspace{1cm}} = \underline{\hspace{1cm}} [E_{rm}]$$

$$E_{\text{m}}(\log) = \frac{20 \log (1 + E_{\text{m}}/S_{11})}{20 \log (1 - E_{\text{m}}/S_{11})}$$

$$\frac{20 \log (1 + \frac{E_{\text{m}}}{S_{11}})}{20 \log (1 - \frac{E_{\text{m}}}{S_{11}})} = + \frac{E_{\text{m}}}{S_{11}} \text{ dB}$$

$$\frac{20 \log (1 - \frac{E_{\text{m}}}{S_{11}})}{20 \log (1 + \frac{E_{\text{m}}}{S_{11}})} = - \frac{E_{\text{m}}}{S_{11}} \text{ dB}$$

PART D — Total Phase Errors

$$E_{rp} = \text{Arcsin}[(E_{rm} - (A_m \times S11))/S11] + A_p$$

$$\text{Arcsin}[(\frac{\quad}{\quad} - (\frac{\quad}{\quad} \times \frac{\quad}{\quad})) / \frac{\quad}{\quad}] + \frac{\quad}{\quad} = \pm \frac{\quad}{\quad}^\circ$$

1. Enter the value from Figure 2-1 as a positive dB value. Convert to linear using the formula: $\text{Linear Value} = 10^{(\text{dB value}/20)} - 1$.

Table 2-5. Transmission Measurement Uncertainty Worksheet

PART A — Analyzer Performance:

In the columns below, enter the values for each term. Values are obtained from Table 2-3 and Figure 2-1.

Error Term	Symbol	dB Value	Linear Value
Crosstalk ¹	C		_____
Transmission tracking	T ₁		_____
Source match (transmission)	M _s		_____
Load match	M _l		_____
Dynamic accuracy			
Magnitude ²	A _m	+ _____	_____
Phase	A _p		_____
Trace noise	N _h		_____
Connector repeatability	R _c		_____
Cable Reflection Magnitude			
Stability	S _r		_____
Cable Transmission Phase			
Stability (Degrees)	S _t		_____

PART B — DUT Performance

In the columns below, enter the calculated or measured performance of the DUT.

Performance Parameter	dB Value	Linear Value (10 ^{dB Value/20})
S11	_____	_____
S21	_____	_____
S12	_____	_____
S22	_____	_____

PART C — Total Magnitude Errors (Systematic and Random)

Systematic Errors

In the spaces provided, enter the required linear values from Parts A and B. Then combine these errors to obtain the total sum of systematic errors.

C _____ = _____ [k]
T₁ x S21 _____ x _____ = _____ [l]
M_s x S11 x S21 _____ x _____ = _____ [m]
(S_r + M_l) x S21 x S22 (_____ + _____) x _____ = _____ [n]
A_m x S21 _____ x _____ = _____ [o]
Total Systematic Errors: k + l + m + n + o = _____ [S]

Random Errors

Enter the required linear values from Parts A and B. Combine these errors in a root sum of the squares (RSS) fashion to obtain a total sum of random errors.

3 x N_h x S21 3x _____ x _____ = _____ [x]
R_c x S21 x (1 + S11) _____ x _____ x (1 + _____) = _____ [y]
R_c x S21 x (1 + S22) _____ x _____ x (1 + _____) = _____ [z]

Total Random Errors

$\sqrt{x^2 + y^2 + z^2}$ $\sqrt{\text{_____} + \text{_____} + \text{_____}}$ = _____ [R]

TOTAL MAGNITUDE ERRORS:

E_{tm}(linear) = S + R _____ + _____ = _____ E_{tm}
E_{tm}(log) = 20 Log (1 + E_{tm}/S21) 20 Log (1 + _____ / _____) = + _____ dB
20 Log (1 - E_{tm}/S21) 20 Log (1 - _____ / _____) = - _____ dB

PART D — Total Phase Errors

E_{tp} = Arcsin[(E_{tm} - (A_m x S21))/S21] S_t + A_p
Arcsin[(_____ - (_____ x _____) / _____] + _____ + _____ = ± _____ °

1. Use the value listed in Table 2-3 or measure (using the instructions provided in "Determining Crosstalk," earlier in this chapter).
1. Enter the value from Figure 2-1 as a positive dB value. Convert to linear using the formula: Linear Value = 10^{dB value/20} - 1.

EXAMPLE

Table 2-4. Reflection Measurement Uncertainty Worksheet

PART A — Analyzer Performance

Frequency: 1.0 GHz

In the columns below, enter the values for each term. Values are obtained from Table 2-3 and Figure 2-1.

Error Term	Symbol	dB Value	Linear Value
Directivity	D		<u>.01</u>
Reflection tracking	T_r		<u>.0233</u>
Source match (reflection)	M_s		<u>.0316</u>
Load match	M_l		<u>.0718</u>
Dynamic accuracy			
Magnitude ¹	A_m	+ <u>.05</u>	<u>.0058</u>
Phase	A_p		<u>.3</u>
Trace noise	N_h		<u>.0007</u>
Connector repeatability	R_c		<u>.0006</u>

PART B — DUT Performance

In the columns below, enter the calculated or measured performance of the DUT.

Performance Parameter	dB Value	Linear Value (10 ^{dB Value/20})
S11	<u>-22</u>	<u>.08</u>
S21	<u>-20</u>	<u>.1</u>
S12	<u>-20</u>	<u>.1</u>

PART C — Total Magnitude Errors (Systematic and Random)

Systematic Errors

In the spaces provided, enter the required linear values from Parts A and B. Then combine these errors to obtain the total sum of systematic errors.

D									
$T_r \times S11$									<u>.01</u> [k]
$M_s \times S11 \times S11$									<u>.001864</u> [l]
$M_l \times S21 \times S12$	<u>.0316</u>	<u>.0233</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.000202</u> [m]
$A_m \times S11$	<u>.0708</u>	<u>.1</u>	<u>.0058</u>	<u>.1</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.000708</u> [n]
									<u>.000464</u> [o]
Total Systematic Errors: k + l + m + n + o									<u>.013238</u> [S]

Random Errors

Enter the required linear values from Parts A and B. Combine these errors in a root sum of the squares (RSS) fashion to obtain a total sum of random errors.

$3 \times N_h \times S11$									
$R_c \times (1 + 2 \times S11 + S11^2)$									<u>.00168</u> [x]
$R_c \times S21 \times S12$	<u>.0006</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.08</u>	<u>.0007</u> [y]
	<u>.0006</u>	<u>.1</u>	<u>.1</u>	<u>.1</u>	<u>.1</u>	<u>.1</u>	<u>.1</u>	<u>.1</u>	<u>.000006</u> [z]

Total Random Errors

$$\sqrt{x^2 + y^2 + z^2} = \sqrt{2.822 \times 10^{-6} + 4.9 \times 10^{-7} + 3.6 \times 10^{-11}} = .00182 \text{ [R]}$$

TOTAL MAGNITUDE ERRORS:

$$E_{m(\text{linear})} = S + R = .01328 + .00182 = .01506 \text{ [E}_{m\text{]}}$$

$$E_{m(\text{log})} = 20 \log(1 + E_{m(\text{linear})}/S11) = 20 \log(1 + .01506/.08) = +1.50 \text{ dB}$$

$$20 \log(1 - E_{m(\text{linear})}/S11) = 20 \log(1 - .01506/.08) = -1.81 \text{ dB}$$

PART D — Total Phase Errors

$$E_{rp} = \arcsin[(E_{m(\text{linear})} - (A_m \times S11))/S11] + A_p$$

$$\arcsin[(.01506 - (.0058 \times .08))/.08] + .3 = \pm 10.8^\circ$$

1. Enter the value from Figure 2-1 as a positive dB value. Convert to linear using the formula: Linear Value = 10^(dB value/20) - 1.

EXAMPLE

Table 2-5. Transmission Measurement Uncertainty Worksheet

PART A — Analyzer Performance:

Frequency 1.0 GHz

In the columns below, enter the values for each term. Values are obtained from Table 2-3 and Figure 2-1.

Error Term	Symbol	dB Value	Linear Value
Crosstalk ¹	C		<u>.00001</u>
Transmission tracking	T _t		<u>.0233</u>
Source match (transmission)	M _s		<u>.0708</u>
Load match	M _l		<u>.0708</u>
Dynamic accuracy			
Magnitude ²	A _m	<u>+ .05</u>	<u>.0058</u>
Phase	A _p		<u>.3</u>
Trace noise	N _h		<u>.0007</u>
Connector repeatability	R _c		<u>.0006</u>
Cable Reflection Magnitude			
Stability	S _r		<u>.001</u>
Cable Transmission Phase			
Stability (Degrees)	S _t		<u>.05</u>

PART B — DUT Performance

In the columns below, enter the calculated or measured performance of the DUT.

Performance Parameter	dB Value	Linear Value (10 ^{dB Value/20})
S11	<u>-22</u>	<u>.08</u>
S21	<u>-20</u>	<u>.1</u>
S12	<u>-20</u>	<u>.1</u>
S22	<u>-23</u>	<u>.071</u>

PART C — Total Magnitude Errors (Systematic and Random)

Systematic Errors

In the spaces provided, enter the required linear values from Parts A and B. Then combine these errors to obtain the total sum of systematic errors.

$$\begin{aligned}
 C &= \underline{.00001} \text{ [k]} \\
 T_t \times S21 &= \underline{.0233} \times \underline{.1} = \underline{.00233} \text{ [l]} \\
 M_s \times S11 \times S21 &= \underline{.0708} \times \underline{.08} \times \underline{.1} = \underline{.00566} \text{ [m]} \\
 (S_r + M_l) \times S21 \times S22 &= (\underline{.001} + \underline{.0708}) \times \underline{.1} \times \underline{.071} = \underline{.00051} \text{ [n]} \\
 A_m \times S21 &= \underline{.0058} \times \underline{.1} = \underline{.00058} \text{ [o]} \\
 \text{Total Systematic Errors: } k + l + m + n + o &= \underline{.004} \text{ [S]}
 \end{aligned}$$

Random Errors

Enter the required linear values from Parts A and B. Combine these errors in a root sum of the squares (RSS) fashion to obtain a total sum of random errors.

$$\begin{aligned}
 3 \times N_h \times S21 &= 3 \times \underline{.0007} \times \underline{.1} = \underline{.00021} \text{ [x]} \\
 R_c \times S21 \times (1 + S11) &= \underline{.0006} \times \underline{.1} \times (1 + \underline{.08}) = \underline{.00065} \text{ [y]} \\
 R_c \times S21 \times (1 + S22) &= \underline{.0006} \times \underline{.1} \times (1 + \underline{.071}) = \underline{.00064} \text{ [z]}
 \end{aligned}$$

Total Random Errors

$$\sqrt{x^2 + y^2 + z^2} = \sqrt{4.41 \times 10^{-8} + 4.2 \times 10^{-9} + 4.129 \times 10^{-9}} = \underline{.000229} \text{ [R]}$$

TOTAL MAGNITUDE ERRORS:

$$E_{tm}(\text{linear}) = S + R$$

$$E_{tm}(\log) = 20 \log(1 + E_{tm}/S21)$$

$$20 \log(1 - E_{tm}/S21)$$

$$\begin{aligned}
 &\underline{.004} + \underline{.000229} = \underline{.004229} E_{tm} \\
 20 \log(1 + \underline{.004229} / \underline{.1}) &= + \underline{.36} \text{ dB} \\
 20 \log(1 - \underline{.004229} / \underline{.1}) &= - \underline{.38} \text{ dB}
 \end{aligned}$$

PART D — Total Phase Errors

$$E_p = \arcsin[(E_{tm} - (A_m \times S21))/S21] S_t + A_p$$

$$\arcsin[(\underline{.004229} - (\underline{.0058} \times \underline{.1})) / \underline{.1}] + \underline{.05} + \underline{.3} = \pm \underline{2.44}^\circ$$

1. Use the value listed in Table 2-3 or measure (using the instructions provided in "Determining Crosstalk," earlier in this chapter).
1. Enter the value from Figure 2-1 as a positive dB value. Convert to linear using the formula: Linear Value = 10^(dB Value/20) - 1.

REFLECTION UNCERTAINTY EQUATIONS

This page shows how E_{rm} is derived from analysis of the system error model shown in Figure 2-3.

Total Reflection Magnitude Uncertainty (E_{rm})

An analysis of the error model (Figure 2-3) yields an equation for the reflection magnitude uncertainty. The equation contains all of the first order terms and the significant second order terms. The three terms under the radical are random and are combined on a root sum of the squares (RSS) basis. The terms in the systematic error group are combined on a worst case basis. In all cases, the error terms and the S-parameters are treated as linear absolute magnitudes.

$$E_{rm}(\log) = 20\log(1 \pm E_{rm}/S_{11})$$

where

$$E_{rm} = S_r + \sqrt{X_r^2 + Y_r^2 + Z_r^2}$$

$$S_r = \text{systematic error} = D + T_r \times S_{11} + M_s \times S_{11}^2 + M_l \times S_{21} \times S_{12} + A_m \times S_{11}$$

$$X_r = \text{random trace noise} = 3 \times N_h \times S_{11}$$

$$Y_r = \text{random port 1 repeatability} = R_c \times (1 + 2 S_{11} + S_{11}^2)$$

$$Z_r = \text{random port 2 repeatability} = R_c \times S_{21} \times S_{12}$$

Total Reflection Phase Uncertainty (E_{rp})

Reflection phase uncertainty is determined from a comparison of the magnitude uncertainty with the test signal magnitude. The worst case phase angle is computed. The result is combined with phase dynamic accuracy.

$$E_{rp} = \arcsin ((E_{rm} - A_m \times S_{11})/S_{11}) + A_p$$

TRANSMISSION UNCERTAINTY EQUATIONS

This page shows how E_{tm} is derived from analysis of the system error model shown in Figure 2-3.

Total Transmission Magnitude Uncertainty (E_{tm})

An analysis of the error model in Figure 2-3 yields an equation for the transmission magnitude uncertainty. The equation contains all of the first order terms and some of the significant second order terms. The three terms under the radical are random and are combined on an RSS basis. The terms in the systematic error group are combined on a worst case basis. In all cases, the error terms are treated as linear absolute magnitudes.

$$E_{tm}(\log) = 20 \log(1 \pm E_{tm} / S_{21})$$

where

$$E_{tm} = S_t + \sqrt{X_t^2 + Y_t^2 + Z_t^2}$$

$$S_t = \text{systematic error} = C + T_t \times S_{21} + M_s \times S_{11} \times S_{21} + (M_l + S_r) \times S_{21} \times S_{22} + A_m \times S_{21}$$

$$X_t = \text{random high-level noise} = 3 \times N_h \times S_{21}$$

$$Y_t = \text{random port 1 repeatability} = R_c \times S_{21} + R_c \times S_{11} \times S_{21}$$

$$Z_t = \text{random port 2 repeatability} = R_c \times S_{21} + R_c \times S_{22} \times S_{21}$$

Total Transmission Phase Uncertainty (E_{tp})

Transmission phase uncertainty is calculated from a comparison of the magnitude uncertainty with the test signal magnitude. The worst case phase angle is computed. This result is combined with the error terms related to phase dynamic accuracy, cable phase stability, and thermal drift of the total system.

$$E_{tp} = \arcsin((E_{tm} - A_m \times S_{21}) / S_{21}) + S_t + A_p$$